

# CENTRE FOR METROLOGY AND ACCREDITATION

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$$m = m_c \frac{1 - \rho_0 / \rho_{ref}}{1 - \rho_0 / \rho_{20}}$$

$$u^2(m_x) = u^2(m_R) + u^2(\rho_a)(V_X - V_R)^2 + \rho_a^2 [u^2(V_X) + u^2(V_R)] + u^2(f)(I_X - I_R)^2$$

$$+ f^2 u^2(I_X - I_R) + 2 \frac{\partial m_x}{\partial m_R} \frac{\partial m_x}{\partial V_R} u(m_R, V_R)$$

$$u^2(m_x) = u^2(m_R) + u^2(\rho_a)(V_X - V_R)^2 + \rho_a^2 [u^2(V_X) + u^2(V_R)] + u^2(f)(I_X - I_R)^2$$

$$+ f^2 u^2(I_X - I_R) - 2 \rho_a \rho_a u^2(V_R)$$

$$u^2(m_{X,c}) = u^2(m_{R,c}) \frac{u^2(\rho_a)}{(1 - \rho_0 / \rho_{ref})^2} (V_X - V_R)^2 \frac{u^2(\rho_a)}{(1 - \rho_0 / \rho_{ref})^2} u^2(V_X) + u^2(V_R)$$

$$+ u^2(f_C)(I_X - I_R)^2 + f_C^2 u^2(I_X - I_R)$$

$$2 \frac{m_{X,c}}{m_{R,c}} \frac{m_{X,c}}{V_R} u(m_{R,c}, V_R) u^2(\rho_a)(u^2(V_X) + u^2(V_R))$$

$$m_{R,C} = m_{ST,C} \frac{(\rho_a - \rho_0)(V_R - V_S)}{1 - \rho_0 / \rho_{ref}} f_C I_R I_S$$

$$m_{X,C} = m_{R,C} \frac{(\rho_a - \rho_0)(V_X - V_R)}{1 - \rho_0 / \rho_{ref}} f_C I_X I_R$$

$$f_x(I) = 1 - E(I)/I$$

$$u(x_i, x_j) = \frac{x_i}{x_k} \frac{x_j}{x_k} u^2(x_k)$$

$$\frac{F}{g} = m_t (1 - \frac{\rho_a}{\rho_t})$$

$$m_x = m_R \frac{\rho_a(V_X(t) - V_R(0))}{f(I_X - I_R)}$$

$$u^2(E) = u^2(I(m_t)) + I^2(m_t) \left( \frac{u^2(\rho_a)}{I} + \frac{\rho_a^2}{I} u^2(\rho_a) \right)$$

$$u^2(m_t) = u^2(I) + 2I(m_t)^2 \frac{\rho_a \rho_a}{I} u^2(\rho_a)$$

## Basic formulas for mass calibration

Kari Riski



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**BASIC FORMULAS FOR MASS CALIBRATION**

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## 1. Introduction

This document gives basic formulas for weight and balance calibration. Formulas are expressed both in terms of the true mass and in terms of the conventional mass. The purpose of this document is to clarify the difference of these quantities. More detailed formulas have been given in elsewhere /1-5/.

## 2. Weight calibration

### 2.1 Conventional mass

The conventional mass of a body /1/ is equal to the mass,  $m_c$  of a standard that balances this body at conventionally chosen conditions:

- temperature  $t_{20} = 20^\circ\text{C}$
- air density  $\rho_0 = 1.2 \text{ kg/m}^3$  (at  $20^\circ\text{C}$ )
- density of the standard  $\rho_{ref} = 8000 \text{ kg/m}^3$ .

The unit of the conventional mass is the kilogram.

According to this definition the relation between the true mass  $m$  of the body and its conventional mass  $m_c$  is the following:

$$m = m_c \frac{1 - \rho_0 / \rho_{ref}}{1 - \rho_0 / \rho_{20}} \quad (1)$$

$$m = m_c - \rho_0 \left( \frac{m_c}{\rho_{ref}} - V(t_{20}) \right) \quad (1')$$

$$m_c = m \frac{1 - \rho_0 / \rho_{20}}{1 - \rho_0 / \rho_{ref}} \quad (2')$$

$$m_c = \left( 1 - \frac{\rho_0}{\rho_{ref}} \right)^{-1} (m - \rho_0 V(t_{20})) \quad (2'')$$

Where:

$V(t_{20}) =$  volume of the weight at reference temperature  $t_{20} = 20^\circ\text{C}$ .

$\rho_{20} = m/V(t_{20})$  is the density of the weight at the reference temperature.

The formulas are given both in terms of volume and in terms of density. The equations in (1) and (2) do not contain any approximations.

## 2.2 True mass difference

Two weights, the test weight  $m_X$  and reference weight  $m_R$  are compared with an ideal mass comparator. The mass difference between the weights is a sum of the air buoyancy difference and the indication difference (see 3.1):

$$m_X - m_R = \rho_a (V_X(t) - V_R(t)) + f(I_X - I_R)$$

$$f = \frac{(m_s - \rho_{as} V_s)}{\Delta I} \quad (3)$$

Where

$m_X$  = true mass of test weight

$m_R$  = true mass of reference weight

$\rho_a$  = density of air during comparison

$V_R(t)$  = volume of reference weight at temperature  $t$

$V_X(t)$  = volume of test weight at temperature  $t$

$f$  = scale factor

$I_X$  = indication of balance with the test weight

$I_R$  = indication of balance with the reference weight

$m_s$  = mass of sensitivity weight

$V_s$  = volume of sensitivity weight

$\rho_s = m_s / V_s$  = density of the sensitivity weight

$\rho_{as}$  = air density during sensitivity measurement

$\Delta I$  = indication difference due to sensitivity weight

In formula (3) it is assumed that the air density is constant during the comparison and that the centre of gravity for both weights is equal. Other contributions such as convection forces, electrostatic forces and magnetic forces has been neglected.

The definition of the scale factor  $f$  is not unambiguous. Here It is determined by placing the sensitivity weight  $m_s$  on the weighing pan and reading the corresponding indication difference  $\Delta I$ . In principle no adjustment is needed. If the indication difference is adjusted equal to the mass of the sensitivity weight  $\Delta I = m_s$  then  $f = 1 - \rho_{as} / \rho_s$ .

### 2.3 Conventional mass difference:

The conventional mass difference of the two weights derived from (3) is the following:

$$m_{X,c} - m_{R,c} = \frac{(\rho_a - \rho_0)(V_X(t) - V_R(t)) + \rho_0(V_X(t_0)\gamma_x - V_R(t_0)\gamma_R)(t - t_0)}{1 - \frac{\rho_0}{\rho_{ref}}} + f_C(I_X - I_R)$$

$$f_C = \frac{(m_s - \rho_{as}V_s)}{\left(1 - \frac{\rho_0}{\rho_{ref}}\right)\Delta I} = (m_{s,c} - \frac{(\rho_{as} - \rho_0)V_s}{\left(1 - \frac{\rho_0}{\rho_{ref}}\right)\Delta I}) \frac{1}{\Delta I}$$
(4)

Where

- $m_{X,c}$  = conventional mass of test weight
- $m_{R,c}$  = conventional mass of reference weight
- $\rho_a$  = density of air during comparison
- $\gamma_R$  = volume expansion coefficient of the reference weight
- $\gamma_X$  = volume expansion coefficient of the test weight
- $f_C$  = scale factor
- $m_{s,c}$  = conventional mass of sensitivity weight

The scale factor  $f_c$  is the coefficient between conventional mass and the corresponding indication. Its value is different from the scale factor for the true mass. If the indication difference  $\Delta I$  is adjusted equal to  $m_{s,c}$  then  $f_c \approx 1 - (\rho_{as} - \rho_0)/\rho_s$ .

### 2.4 True mass and its uncertainty

From (3) the following equation for  $m_X$  can be derived. If the mass of the reference weight has been determined in a comparison with a higher order mass standard  $m_{ST}$  then an analogous formula for  $m_R$  can be derived:

$$m_R = m_{ST} + \rho_{ar}(V_R - V_{ST}) + f_r(I_R - I_S)$$

$$m_X = m_R + \rho_a(V_X - V_R) + f(I_X - I_R)$$
(5)

Where:

- $m_{ST}$  = mass of the higher order mass standard
- $V_{ST}$  = volume of the higher order mass standard
- $\rho_{ar}$  = density of air when  $m_R$  was calibrated

The covariance between the true mass and the volume of the reference weight  $u(m_R, V_R)$  has the following form:

$$u(m_R, V_R) = \frac{\partial m_R}{\partial V_R} \frac{\partial V_R}{\partial V_R} u^2(V_R) = \rho_{ar} u^2(V_R)$$
(6)

From (5) the square of the standard uncertainty  $u(m_X)$  of  $m_X$  is:

$$\begin{aligned}
 u^2(m_X) &= u^2(m_R) + u^2(\rho_a)(V_X - V_R)^2 + \rho_a^2 [u^2(V_X) + u^2(V_R)] + u^2(f)(I_X - I_R)^2 \\
 &+ f^2 u^2(I_X - I_R) + 2 \frac{\partial m_X}{\partial m_R} \frac{\partial m_X}{\partial V_R} u(m_R, V_R) \\
 u^2(m_X) &= u^2(m_R) + u^2(\rho_a)(V_X - V_R)^2 + \rho_a^2 [u^2(V_X) + u^2(V_R)] + u^2(f)(I_X - I_R)^2 \\
 &+ f^2 u^2(I_X - I_R) - 2\rho_a \rho_{ar} u^2(V_R)
 \end{aligned} \tag{7}$$

Where  $u(x_i)$  is the standard uncertainty of the quantity  $x_i$ .

$u(x_i, x_j) = \sum_k \frac{\partial X_i}{\partial x_k} \frac{\partial X_j}{\partial x_k} u^2(x_k)$  is the covariance between  $x_i$  and  $x_j$ .

The correlation coefficient of  $x_i$  and  $x_j$  is  $r(x_i, x_j) = u(x_i, x_j) / (u(x_i)u(x_j))$ .

The correlation coefficient between  $m_X$  and  $V_X$  is

$$r(m_X, V_X) = \frac{u(m_X, V_X)}{u(m_X)u(V_X)} = \rho_a \frac{u(V_X)}{u(m_X)} \tag{8}$$

It is assumed that there is no other correlation.

## 2.5 The conventional mass and its uncertainty

In the following the same formulas as in the previous section are given in terms of the conventional mass. The conventional mass of the reference weight  $m_{R,C}$  has been determined with a higher order mass standard ( $m_{S,C}, V_S$ ) at air density  $\rho_a$ . The conventional masses can be obtained from the following equations derived from (4):

$$\begin{aligned}
 m_{R,C} &\approx m_{ST,C} + \frac{(\rho_{ar} - \rho_0)(V_R - V_S)}{1 - \frac{\rho_0}{\rho_{ref}}} + f_{Cr}(I_R - I_S) \\
 m_{X,C} &\approx m_{R,C} + \frac{(\rho_a - \rho_0)(V_X - V_R)}{1 - \frac{\rho_0}{\rho_{ref}}} + f_C(I_X - I_R)
 \end{aligned} \tag{9}$$

The conventional mass  $m_{R,C}$  and the volume  $V_R$  are correlated their covariance  $u(m_{R,C}, V_R)$  is:

$$u(m_{R,C}, V_R) = \frac{\partial m_{R,C}}{\partial V_R} \frac{\partial V_R}{\partial V_R} u^2(V_R) = \frac{(\rho_{ar} - \rho_0)}{1 - \frac{\rho_0}{\rho_{ref}}} u^2(V_R) \tag{10}$$

The standard uncertainty  $u(m_{X,c})$  can be obtained from the formula:

$$\begin{aligned}
 u^2(m_{X,c}) = & u^2(m_{R,c}) + \frac{u^2(\rho_a)}{(1 - \frac{\rho_0}{\rho_{ref}})^2} (V_X - V_R)^2 + \frac{(\rho_a - \rho_0)^2}{(1 - \frac{\rho_0}{\rho_{ref}})^2} [u^2(V_X) + u^2(V_R)] \\
 & + u^2(f_C)(I_X - I_R)^2 + f_C^2 u^2(I_X - I_R) \\
 & + 2 \frac{\partial m_{X,c}}{\partial m_{R,c}} \frac{\partial m_{X,c}}{\partial V_R} u(m_{R,c}, V_R) + u^2(\rho_a)(u^2(V_X) + u^2(V_R))
 \end{aligned} \tag{11}$$

Both the covariance term (second term on last line) and a second order term (last term) have been included. The second order term is significant only if  $V_X \approx V_R$  and  $\rho_a \approx \rho_0$ .

If we assume that the constant  $1 - \rho_0 / \rho_{ref} \approx 1$  then

$$\begin{aligned}
 u^2(m_{X,c}) \approx & u^2(m_{R,c}) + u^2(a)(V_X - V_R)^2 + (\rho_a - \rho_0)^2 [u^2(V_X) + u^2(V_R)] + u^2(f_C)(I_X - I_R)^2 \\
 & + f_C^2 u^2(I_X - I_R)^2 - 2(\rho_a - \rho_0)(\rho_{ar} - \rho_0)u^2(V_R) + u^2(a)(u^2(V_X) + u^2(V_R))
 \end{aligned} \tag{12}$$

Also  $m_{X,C}$  and  $V_X$  are correlated the correlation coefficient is

$$r(m_{X,C}, V_X) = \frac{u(m_{X,C}, V_X)}{u(m_{X,C})u(V_X)} = \frac{(\rho_a - \rho_0)}{1 - \frac{\rho_0}{\rho_{ref}}} \frac{u(V_X)}{u(m_{X,C})} \tag{13}$$

## 2.6 Mass expressed in terms of density

From (5) the true mass  $m_x$  expressed in terms of density is

$$m_x = m_R \frac{1 - \rho_a / \rho_R}{1 - \rho_a / \rho_X} + f(I_X - I_R) \frac{1}{1 - \rho_a / \rho_X} \tag{5'}$$

From (9) The corresponding formula for the conventional mass is

$$m_{x,c} = m_{R,c} \frac{1 - \rho_a / \rho_R}{1 - \rho_a / \rho_X} \frac{1 - \rho_0 / \rho_X}{1 - \rho_0 / \rho_R} + f_c(I_X - I_R) \frac{1 - \rho_0 / \rho_X}{1 - \rho_a / \rho_X} \tag{9'}$$



The covariance between mass and density is approximately:

$$u(m_{X,c}, \rho_X) = \frac{\partial m_{X,c}}{\partial \rho_X} \frac{\partial \rho_X}{\partial \rho_X} u^2(\rho_X) = -m_{X,c} \frac{\rho_a}{\rho_X(\rho_X - \rho_a)} u^2(\rho_X) \quad (8')$$

The covariance between conventional mass and density is approximately:

$$u(m_{X,c}, \rho_X) = \frac{\partial m_{X,c}}{\partial \rho_X} \frac{\partial \rho_X}{\partial \rho_X} u^2(\rho_X) = -m_{X,c} \frac{(\rho_a - \rho_0)}{(\rho_X - \rho_0)(\rho_X - \rho_a)} u^2(\rho_X) \quad (10')$$

### 3. Mass comparators

#### 3.1 Model for a mass comparator

Gravitational force  $F$  due to a weight  $m_t$  is:

$$\frac{F}{g} = m_t \left(1 - \frac{\rho_a}{\rho_t}\right) \quad (14)$$

$m_t$  = mass of weighted object  
 $\rho_t$  = density of weighted object  
 $\rho_a$  = air density during weighing  
 $F$  = vertical force to the weighing pan  
 $g$  = acceleration of free fall

The indication  $I$  of an ideal balance when loaded with mass  $m_t$  is directly proportional to the gravitational force:

$$I(m_t) = \alpha \cdot \frac{F}{g} = \alpha \cdot m_t \left(1 - \rho_a / \rho_t\right) \quad (15)$$

Where:

$I$  = indication of the balance  
 $\alpha$  = calibration constant

The calibration constant  $\alpha$  is determined by weighing the adjustment weight  $m_{cs}$  and by setting the display equal to  $m_{cs}$ .

$$m_{cs} = \alpha \cdot m_s \left(1 - \rho_{as} / \rho_s\right) = \alpha \cdot m_{cs} \frac{1 - \rho_0 / \rho_{ref}}{1 - \rho_0 / \rho_s} \left(1 - \rho_{as} / \rho_s\right) \quad (16)$$

$$\alpha^{-1} = \left[ \frac{1 - \rho_0 / \rho_{ref}}{1 - \rho_0 / \rho_s} \left(1 - \rho_{as} / \rho_s\right) \right] \quad (17)$$

Where:

$\rho_{as}$  = air density during adjustment  
 $m_s$  = mass of the adjustment weight  
 $m_{cs}$  = conventional mass of adjustment weight  
 $\rho_s$  = density of adjustment weight

By substituting  $\alpha$  to (15) and solving  $m_t$  we have

$$m_t = \frac{1 - \rho_{as} / \rho_s}{1 - \rho_a / \rho_t} \cdot \frac{1 - \rho_0 / \rho_{ref}}{1 - \rho_0 / \rho_s} I(m_t) \quad (18)$$

$$m_t \approx \left[ 1 + \left( \frac{1}{\rho_t} - \frac{1}{\rho_s} \right) \rho_a - \frac{\rho_{as} - \rho_a}{\rho_s} \right] \cdot \left[ \frac{1 - \rho_0 / \rho_{ref}}{1 - \rho_0 / \rho_s} \right] \cdot I(m_t) \quad (18')$$

In (18)  $m_t$  is can be expressed in terms of conventional mass  $m_{ct}$ .

$$m_t = m_{ct} \frac{(1 - \rho_0 / \rho_{ref})}{1 - \rho_0 / \rho_t} \quad (19)$$

When  $m_{ct}$  is solved we get

$$m_{tc} = \frac{1 - \rho_{as} / \rho_s}{1 - \rho_a / \rho_t} \cdot \frac{1 - \rho_0 / \rho_t}{1 - \rho_0 / \rho_s} \cdot I(m_t) \quad (20)$$

$$m_{tc} \approx \left[ 1 + \left( \frac{1}{\rho_t} - \frac{1}{\rho_s} \right) \cdot (\rho_a - \rho_0) - \frac{\rho_{as} - \rho_a}{\rho_s} \right] \cdot I(m_t) \quad (20')$$

Corrections to the approximations (18') and (20') are of the order of  $(\rho_a / \rho_0)^2 \cdot I(m_t)$ . In practice they can be neglected. If the balance is adjusted before the measurement then  $\rho_{as} \approx \rho_a$  and the last terms on the right hand side of (18') and (20') can be neglected.

When calibrating the balance the following models are possible:

- a) The error of indication of the balance without air buoyancy correction  $E$  is determined:

$$E = I(m_{tc}) - m_{tc} + \delta I(m_{tc}) + \delta m_{tc} \quad (21)$$

where  $\delta I(m_t)$  is a correction due to nonidealities of the balance (eccentricity, magnetic effects etc.) at load  $m_t$  and  $\delta m_{tc}$  is zero correction due to air buoyancy. It is included to be taken into account in uncertainty calculations.

- b) The error of air buoyancy corrected indication is determined:

$$E = I(m_t) \cdot \frac{1 - \rho_{as} / \rho_s}{1 - \rho_a / \rho_t} \cdot \frac{1 - \rho_{a0} / \rho_{ref}}{1 - \rho_{a0} / \rho_s} - m_t + \delta I(m_t) \quad (22)$$

or

$$E = I(m_{tc}) \cdot \frac{1 - \rho_{as} / \rho_s}{1 - \rho_a / \rho_t} \cdot \frac{1 - \rho_{a0} / \rho_t}{1 - \rho_{a0} / \rho_s} - m_{tc} + \delta I(m_{tc}) \quad (23)$$

In practice the formula (23) is preferred because the density and the (true) mass of the weight are strongly correlated.

### 3.2 Uncertainty of the error of indication

For uncertainty calculations In (22) and (23) it can be assumed that the density of the sensitivity weight is equal to the reference density:  $\rho_s = \rho_{ref}$ . In addition the following approximations will be made:

$$E \approx I(m_t) + I(m_t)(\rho_a / \rho_t - \rho_{as} / \rho_{ref}) - m_t + \delta I(m_t) \quad (24)$$

and

$$E \approx I(m_{tc}) + I(m_{tc})((\rho_0 - \rho_{as}) / \rho_{ref} + (\rho_a - \rho_0) / \rho_t) - m_{tc} + \delta I(m_{tc}) \quad (25)$$

The uncertainty of  $E$  from (24) is calculated assuming that  $\rho_{as}$  is constants and  $I(m_t) \approx m_t \approx m_{t,c}$ . The air density at the time when the weights were calibrated is  $\rho_{at}$ .

$$u^2(E) = u^2(I(m_t)) + I^2(m_t) \cdot \left[ \frac{u^2(\rho_a)}{\rho_t^2} + \frac{\rho_a^2}{\rho_t^4} \cdot u^2(\rho_t) \right] + u^2(m_t) + u^2(\delta I) - 2I(m_t)^2 \frac{\rho_a \rho_{at}}{\rho_t^4} u^2(\rho_t) \quad (26)$$

Here the covariance term with (8')

$$2 \frac{\partial E}{\partial m_t} \frac{\partial E}{\partial \rho_t} u(m_t, \rho_t) \approx 2 \cdot (-1) \cdot \left[ -I(m_t) \frac{\rho_a}{\rho_t^2} \right] \cdot \left[ -\frac{\rho_{at}}{\rho_t^2} m_t u^2(\rho_t) \right] \quad (27)$$

has been included.

For conventional mass from (25):

$$u^2(E) = u^2(I(m_{tc})) + I^2(m_{tc}) \cdot \left[ \frac{u^2(\rho_a)}{\rho_t^2} + \frac{(\rho_a - \rho_0)^2}{\rho_t^4} \cdot u^2(\rho_t) \right] + u^2(m_{tc}) + u^2(\delta I) - 2I(m_t)^2 \frac{(\rho_a - \rho_0)(\rho_{at} - \rho_0)}{\rho_t^4} u^2(\rho_t) \quad (28)$$

Also here the covariance term with (10')

$$2 \frac{\partial E}{\partial m_{tc}} \frac{\partial E}{\partial \rho_t} u(m_t, \rho_t) = 2 \cdot (-1) \cdot \left[ -I(m_t) \frac{(\rho_a - \rho_0)}{\rho_t^2} \right] \cdot \left[ -\frac{(\rho_{at} - \rho_0)}{\rho_t^2} m_t u^2(\rho_t) \right] \quad (29)$$

has been included.

Formulas (26) and (28) give practically identical values for the uncertainty of the error  $E$ .

### 3.3 Modified scale factor

Usually the mass of the weighed object is of primary interest. In addition to the mass the balance indication also depends on air density and on the density of the weighed object. In principle the density dependence can be corrected. Because a balance is not an ideal instrument some additional corrections are needed. One possibility is to divide the scale factor into two components. From (22) if we assume that  $\rho_s = \rho_{ref}$  we have

$$m_t = I \cdot \frac{1 - \rho_{as} / \rho_{ref}}{1 - \rho_a / \rho_t} - E(I) = f(\rho_a, \rho_t) f_x(I) \cdot I \quad (30)$$

where the density dependent scale factor  $f(\rho_a, \rho_t)$  is

$$f(\rho_a, \rho_t) = \frac{1 - \rho_{as} / \rho_{ref}}{1 - \rho_a / \rho_t} \quad (31)$$

and the instrumental scale factor  $f_x$  is

$$f_x(I) \approx 1 - E(I) / I \quad (32)$$

The instrumental scale factor will be determined in calibration. It contains e.g. non-linearity of the indication, eccentric loading, temperature dependence of indication. Its value is not however constant with time.

It is important to note that a balance (or a mass comparator) measures force to the weighing pan. It can not directly take into account changes in air density, in the density of the measured object or changes in gravitational acceleration. Changes in air density or in gravitation can be taken into account by adjusting the reading of the balance with an external or internal sensitivity weight. In some balances this is done automatically.

The balance indication is closer to the conventional mass than to the true mass. In many cases the indication can directly used as the conventional mass. This is normally not valid for true mass.

**References:**

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- /3/ EA Guidelines on the calibration of nonautomatic weighing instruments, 2<sup>nd</sup> Predraft , 2002, EA-LC Expert's Group Mechanical Measurements
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